ROTATING FLUIDS

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subjects

* Taylor Proudman theory

- *The Ekman layer; Ekman layer instability
- * Inertial waves (Rossby waves)
- * Shallow water equations Barotropic instability

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Rayleigh criterion circular flow (vortices)
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Baroclinic instability

ROTATING FLUIDS

- Geophysical flows : Earth Oceans and atmosphere, mantel convection,
- Astrophysical flows, Other planetary atmospheres, accretion disks
- Industrial flows :

mixing of chemical compounds in rotating containers, *centrifuges* in nuclear power industry *coating* of material on disks (so called Spin-coating) etc.

ROTATING FLUIDS (intro)

We consider a homogenous fluid in solid body rotation with density ρ and viscosity $\nu,$ and use the Cartesian coordinate system

$\bar{\mathbf{x}} = x\bar{\mathbf{i}} + y\bar{\mathbf{j}} + z\bar{\mathbf{k}}$

with the rotation vector in the k direction, the rotation vector is $\Omega = \Omega_z \mathbf{k} = (0, 0, \Omega_z)$. Suppose a point of mass m at a position x experiences a force **F**, then according to the second law of Newton :

$$m\left[\frac{d^2\bar{\mathbf{x}}}{dt^2} + 2\bar{\Omega} \times \frac{d\bar{\mathbf{x}}}{dt} + \bar{\Omega} \times \bar{\Omega} \times \bar{\mathbf{x}}\right] = \bar{\mathbf{F}}$$

resp. acceleration, Coriolis force and centrifugal force

Suppose $\mathbf{u}(\mathbf{x},t)$ is the fluid velocity with respect to the inertial system, the Navier-Stokes equations is with

$$\bar{\Omega} \times (\bar{\Omega} \times \bar{\mathbf{x}}) = -\nabla (\frac{1}{2}\Omega^2 r^2), \ r = \sqrt{x^2 + y^2}$$
$$\rho \left[\frac{\partial \bar{\mathbf{u}}}{\partial t} + (\bar{\mathbf{u}} \cdot \nabla) \bar{\mathbf{u}} + 2\Omega \times \bar{\mathbf{u}} - \nabla (\frac{1}{2}\Omega^2 r^2) \right] = -\nabla \rho + \rho \bar{\mathbf{g}} + \mu \nabla^2 \bar{\mathbf{u}}$$

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For ρ =constant, the gravity force can be written as a potential V, so that the pressure p can be defined as

$$p = \frac{p}{\rho} + V - \frac{1}{2}\Omega^2 r^2$$

we obtain for the Navier Stokes equation in a rotating fluid:

$$\frac{\partial \bar{\mathbf{u}}}{\partial t} + (\bar{\mathbf{u}} \cdot \nabla) \bar{\mathbf{u}} + 2\Omega \times \bar{\mathbf{u}} = -\nabla p + \nu \nabla^2 \bar{\mathbf{u}}$$

and continuity (since ρ =constant) : $\nabla \cdot \mathbf{\bar{u}} = \mathbf{0}$.

Note :The third lhs term is the Coriolis force. There is no distance r with respect to the axis of rotation, The position of the axes **r=0** has no importance for the Coriolis force.

ROTATING FLUIDS Geophysical large scale flows

In order to simplify the NS equation, we can consider the order of magnitude of these numbers for a particular system.

For example consider a large scale geophysical flow the scales are very large O(4000Km), velocities of O(20m/s) (JetStream) and the background rotation $f\approx 10-4$. For the Ro-number this implies

$$Ro pprox rac{20}{4 \ 10^6 \ 10^{-4}} = rac{1}{20} pprox 0.05$$
, i.e. $Ro << 1$.
 $(\Omega T)^{-1} << 1$.

The Ekman number is small in fast rotating and large scale flows (i.e. viscous effects are small, except in the boundary)

E < 1.

The leading order (dimensionless) geostrophic balance equations are:

 $2\mathbf{\bar{k}} \times \mathbf{\bar{u}} = -\nabla \rho$ $\nabla \cdot \mathbf{\bar{u}} = 0$

i.e. balance between the pressure and the coriolis force. (P is constant along stream lines).

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In order to make the NS equation dimensionless we often scale with a characteristic velocity U_{0} , length L, time scale L/U and pressure scale $LU^{2}.$

$$\mathbf{\bar{x}} = L\mathbf{\bar{x}}', t = Tt', \mathbf{\bar{u}} = U\mathbf{\bar{u}}', \mathbf{\bar{p}} = \rho\Omega L Up', \mathbf{\bar{\Omega}} = \Omega_z \mathbf{\bar{k}}$$

After substitution (after omitting the primes) :

 $\frac{1}{\Omega T} \frac{\partial \bar{\mathbf{u}}}{\partial t} + Ro(\bar{\mathbf{u}} \cdot \nabla)\bar{\mathbf{u}} + 2\bar{\mathbf{k}} \times \bar{\mathbf{u}} = -\nabla p + E\nabla^2 \bar{\mathbf{u}}$ $\nabla \cdot \mathbf{v} = 0$

The non dimensional numbers Ro, E and ΩT are :

$$Ro = \frac{U}{\Omega L} = \frac{U^2/L}{\Omega U} \sim \frac{\text{inertia forces}}{\text{Coriolis force}} \quad (\text{Rossby number})$$
$$E = \frac{\nu}{L^2 \Omega} = \frac{\nu U/L^2}{\Omega U} \sim \frac{\text{viscous effects}}{\text{Coriolis force}} \quad (\text{Ekman number})$$
$$T, \text{ is the characteristic flow time} \qquad \Omega T = \frac{2\pi T}{2\pi/\Omega}$$

ROTATING FLUIDS Taylor Proudman theorem

Eliminate the pressure term by taking the curl of $2\bar{\mathbf{k}} \times \bar{\mathbf{u}} = -\nabla p$

$$2\nabla \times (\mathbf{\bar{k}} \times \mathbf{\bar{u}}) = -\nabla \times (\nabla p) = 0$$

with the vector identity

$$\nabla\times(\bar{k}\times\bar{u})=\bar{k}(\nabla\cdot\bar{u})+(\bar{u}\cdot\nabla)\bar{k}-\bar{u}(\nabla\cdot\bar{k})-(\bar{k}\cdot\nabla)\bar{u}$$

and continuity $\nabla \cdot \bar{\mathbf{u}} = \mathbf{0}$

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$$abla ar{\mathbf{u}} = \mathbf{0} \qquad \rightarrow \qquad \frac{\partial ar{\mathbf{u}}}{\partial z} = \mathbf{0}$$

This is the Taylor-Proudman theorem stating that, to leading order ($Ro \ll I$), there are no variations in the velocity along the axes of rotation

(Proudman 1916, Taylor 1923).











ROTATING FLUIDS inertial waves

In the geostrophic approximation Ro<<1 the equations reduce to the linear relation:

 $\nabla \cdot \bar{\mathbf{u}} = 0$ $\frac{\partial \bar{\mathbf{u}}}{\partial t} + 2\mathbf{\Omega} \times \bar{\mathbf{u}} = -\frac{1}{\rho} \nabla p$ $\longrightarrow \quad \frac{\partial^2 \nabla^2 w}{\partial t^2} + 4\Omega^2 \frac{\partial^2 w}{\partial z^2} = 0$

This equation has planar waves as solutions:

$$\bar{\mathbf{u}} = Re(\mathbf{A})e^{i(\bar{\mathbf{k}}\cdot\bar{\mathbf{x}}-\sigma t)}$$
$$p = Re(P)e^{i(\bar{\mathbf{k}}\cdot\bar{\mathbf{x}}-\sigma t)}$$

k the wave vector and σ the frequency







See experiment later on.

EKMAN BOUNDARIES

Ekman boundary Ekman Boundary layers

Consider a geostrophic flow. In the interior the Taylor Proudman theorem holds, so that $\overline{\mathbf{U}}_{\mathbf{I}} = U_I(x, y)$ and $P_I = P_I(x, y)$. At the boundaries there is adjustment to zero velocity ($\overline{\mathbf{u}} = 0$) so that $\frac{\partial \overline{\mathbf{u}}}{\partial z} \neq 0$, and nonzero vertical velocities.

This thin layer is called the Ekman layer :

Vertical gradients are large : $\frac{\partial}{\partial z} >> 1$, or $\frac{\partial}{\partial z} >> 1/\delta$ and $\delta << 1$. In the boundary, we have (*E* for Ekman boundary layer)

$$\Omega^{+\varepsilon} - 2v_E = -\frac{\partial p_E}{\partial x} + E\frac{\partial^2 u_E}{\partial z^2}$$

$$\Omega^{-2}v_E = -\frac{\partial p_E}{\partial y} + E\frac{\partial^2 v_E}{\partial z^2}$$

$$0 = \frac{\partial p_E}{\partial z} + E\frac{\partial^2 w_E}{\partial z^2}$$

$$\frac{\partial u_E}{\partial x} + \frac{\partial v_E}{\partial y} + \frac{\partial w_E}{\partial z} = 0$$

Ekman Boundary layers Since $w_E = O(\delta) \ll 1$, $w(E)/\delta = O(1) \Longrightarrow \frac{P_E}{\delta} + E \frac{w_E}{\delta^2} = 0$ (E<<1) i.e. $\frac{\partial p_E}{\partial z} = 0$

Thus the pressure in the Ekman layer P_E must be equal to the pressure in the interior, P_I for which we know that

$$-2v_I = -\frac{\partial P_I}{\partial x} \quad 2u_I = -\frac{\partial P_i}{\partial y}$$

so that

$$-2v_E = -2v_I + E\frac{\partial^2 u_E}{\partial z^2} \quad 2u_E = 2u_I + E\frac{\partial^2 v_E}{\partial z^2}$$

We solve this by defining a complex velocity

$$\phi = (u_E + iv_E) - (u_I + iv_I) \text{ so that}$$

$$E \frac{\partial^2 \phi}{\partial z^2} = 2i\phi$$





$$U(z) = \frac{U}{V_{\infty}} = -e^{-z} \cos z$$
$$V(z) = \frac{V}{V_{\infty}} = 1 - e^{-z} \cos z$$







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down experiment with a stratified fluid to be discussed shortly.)

Spin-up can exhibit the same type of instability but the techniques

of visualization must be altered slightly.





Ekman Layer instability

The Ekman layer instability has been investigated experimentally and theoretically by Faller JFM 1963-1991 and theoretically by Lilly 1966 see Lingwood 1996, 1997



The instability is related to inflection point instability Cross flow instability related cross flow over aircraft wings,

NOTE: Similar approaches for von Karman rotating disk flow, and Bödewadt flow (i.e. rotating fluid above a stationary disk) see Lingwood JFM 1996, 1997, Saric 2003 Annu. Ann. Rev. Fluid Mech. 2003. 35:413-40





rewriting the Shallow water equations

Integration of the continuity equation from z=0 to $H + \eta$ gives :

$$(H + \eta)\frac{\partial u}{\partial x} + (H + \eta)\frac{\partial v}{\partial y} + w(\eta) + w(0) = 0$$

Since w(0) = 0 and $w(\eta) = \frac{D\eta}{Dt}$ we obtain :

$$\frac{\partial \eta}{\partial t} + \frac{\partial}{\partial x} [u(H+\eta)] + \frac{\partial}{\partial y} [v(H+\eta)] = 0$$

with $h = H + \eta$ this can be written as

$$\frac{Dh}{Dt} + h(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y}) = 0$$

Potential vorticity equationIntermezzoCross differentiation and substitution of the continuity in the Euler
relations directly gives for the vorticity $\bar{\omega} = (0, 0, \omega_z)$, with
 $\omega_z = \frac{\partial \omega}{\partial x} - \frac{\partial u}{\partial y}$: $\frac{\partial \omega_z}{\partial t} + u \frac{\partial \omega_z}{\partial x} + v \frac{\partial \omega_z}{\partial y} + f(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y}) = 0$
with
 $\frac{Dh}{Dt} + h(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y}) = 0.$ This gives the conservation of potential vorticity : $\frac{D\omega_z}{Dt} = \frac{\omega_z + f}{h} \frac{Dh}{Dt}$
or
 $\frac{D}{Dt} \left(\frac{\omega_z + f}{h}\right) = 0$



$$\frac{\partial u'}{\partial t} + U \frac{\partial u'}{\partial x} + v' \frac{\partial U}{\partial y} - fv' = -\frac{1}{\rho_0} \frac{\partial p'}{\partial x}$$
$$\frac{\partial v'}{\partial t} + U \frac{\partial v'}{\partial x} + v' \frac{\partial U}{\partial y} + fu' = -\frac{1}{\rho_0} \frac{\partial p'}{\partial y}$$
$$\frac{\partial u'}{\partial x} + \frac{\partial v'}{\partial y} = 0$$

The last equation admits the use of a streamfunction

$$u' = -\frac{\partial \psi}{\partial y} , \ v' = \frac{\partial \psi}{\partial x}$$

so that after cross differentiation we obtain :

$$\left(\frac{\partial}{\partial t} + U\frac{\partial}{\partial x}\right)\nabla^2\psi + \frac{d}{dy}\left(f - \frac{dU}{dy}\right)\frac{\partial\psi}{\partial x} = 0$$

($abla^2\psi=\omega$, and so deriving the vorticity yields the same result)

(2)

Shallow water equations and barotropic Instability !

Since $L \ll H$ and $w \ll u$, $\frac{\partial w}{\partial z} = 0$ Since $\nu = 0$, u and v don't vary in z direction : $\frac{\partial u}{\partial z} = \frac{\partial v}{\partial z} = 0$.

As a basic state we consider a uniform flow : u = U(y) that satisfies geostrophic balance, i.e. : $fU = -\frac{1}{\rho_0} \frac{dP}{dy}$ Perturbations :

$$u = U(y) + u'(x, y, t)$$

$$v = v'(x, y, t)$$

$$p = P(y) + p'(x, y, t)$$

A perturbation of the form $\psi = \phi(y) \exp[i(lx - \omega t)]$ yields :

$$rac{d^2\phi}{dy^2} - l^2\phi + rac{rac{d}{dy}(f-rac{dU}{dy})}{U-c}\phi = 0 \quad c = \omega/l$$

in which we recognize the Rayleigh equation. It is too difficult to solve this system for its unstable eigenvalues, and we consider the less constraining, integral properties. As for Rayleigh's criterion multiply the ϕ with its complex conjugate ϕ^* to get with boundary conditions $\phi(y = 0) = \phi(y = L) = 0$:

$$-\int_{0}^{L} \left(|\frac{d\phi}{dy}|^{2} + l^{2}|\phi|^{2} \right) dy + \int_{0}^{L} \frac{\frac{d}{dy} \left(f - \frac{dU}{dy} \right)}{U - c} |\phi|^{2} dy = 0$$

The imaginary part of this expression is :

$$c_i \int_0^L \frac{d}{dy} (f - \frac{dU}{dy}) \frac{|\phi|^2}{|U - c|^2} dy = 0$$

Stable flow when
$$c_i = 0$$
.
For $c_i \neq 0 \left[\frac{d}{dy} \left(f - \frac{dU}{dy} \right) \right]$ must change sign for instability !

Note that for f = 0 we recover Rayleigh instability criterion for a shear layer with vorticity $\omega_z = \frac{d^2 U}{dv^2}$.

Further we note that in reality f varies with latitude y., i.e. $f=f_0+\beta y.$ A background vorticity gradient thus changes the stability criterion.



























The coupling between the two layers is via the second term, and depends on the layer depth (pressure)

general procedure: perturbation equations ...



$$\Rightarrow \begin{pmatrix} \left[\frac{\partial}{\partial t} + U\frac{\partial}{\partial x}\right] \left[\nabla^2 \psi_1 + \frac{1}{2}F^2(\psi_2 - \psi_1)\right] + \frac{\partial \psi_1}{\partial x}(\beta + F^2U) = 0 \\ \left[\frac{\partial}{\partial t} - U\frac{\partial}{\partial x}\right] \left[\nabla^2 \psi_2 + \frac{1}{2}F^2(\psi_1 - \psi_2)\right] + \frac{\partial \psi_2}{\partial x}(\beta - F^2U) = 0 \\ \text{substitute } \psi_i = Re\Psi_i e^{i(kx+ly-\omega t)} \\ \Rightarrow \begin{pmatrix} \left[ik(U-c)\right] \left[-K^2\Psi_1 + \frac{1}{2}F^2(\Psi_2 - \Psi_1)\right] + ik\Psi_1(\beta + F^2U) = 0 \\ \left[-ik(U+c)\right] \left[-K^2\Psi_2 + \frac{1}{2}F^2(\Psi_1 - \Psi_2)\right] + ik\Psi_2(\beta - F^2U) = 0 \\ \text{after substracting and adding the equations we get :} & 3 \ cases: \\ \Rightarrow \begin{pmatrix} \left[(U-c)(\frac{1}{2}F^2 + K^2) - (\beta + F^2U)\right]\Psi_1 - \left[F^2(U-c)/2\right]\Psi_2 = 0 \\ \left[F^2(U+c)\right]\Psi_1 - \left[(U+c)(\frac{1}{2}F^2 + K^2) + (\beta - F^2U)\right]\Psi_2 = 0 \end{pmatrix} & \beta=0 \Rightarrow (1) \\ \beta\neq 0 \Rightarrow (2) \\ [A]\Psi_1 + [B]\Psi_2 = 0, \quad [C]\Psi_1 + [D]\Psi_2 = 0 & U=0 \Rightarrow (3) \\ \Rightarrow & AD - BC = 0 \end{pmatrix}$$











 $\partial x + \partial y + \partial z = 0 \qquad p = \bar{p}(y, z) + p'(x, y, z)$ $\frac{\partial \rho}{\partial t} + u \frac{\partial \rho}{\partial x} + v \frac{\partial \rho}{\partial y} + w \frac{\partial \rho}{\partial z} = 0$ Baroclinic instability (on the Eady problem) $w' = -\frac{1}{\rho N^2} \left[\left(\frac{\partial}{\partial z} + U \frac{\partial}{\partial x} \right) \frac{\partial p'}{\partial z} - \frac{dU}{dz} \frac{\partial p'}{\partial x} \right]$ The pressure perturbation equation becomes: $\left(\frac{\partial}{\partial t} + U \frac{\partial}{\partial x} \right) \left[\nabla_H p' - \frac{f^2}{N^2} \frac{\partial^2 p'}{\partial z^2} \right] = 0$

Consider a flow between z=0 and z=H, and p'=P(z) exp(i[kx +ly - ω t])

 $\begin{array}{l} P(z) \mbox{ is solved with } \Delta p = 0 \mbox{ and gives:} \\ P = A \mbox{ cosh } \mu(z/H - 1/2) + B \mbox{ sinh } \mu(z/H - 1/2) \\ \mbox{ with } \mu^2 = (N/f)^2 \ (k^2 + l^2) H = \ R_d^2 \ K^2 \\ \mbox{ w=0 at } z = 0, H \ \dots \end{array}$

$$c = \frac{U_0}{2} \pm \frac{U_0}{\mu} \sqrt{(\frac{\mu}{2} - \tanh\frac{\mu}{2})(\frac{\mu}{2} - \coth\frac{\mu}{2})}$$

Baroclinic instability (on the Eady problem)

Vorticity equation (after cross differentiation and use of continuity) :

$$\frac{\partial \omega}{\partial t} + u \frac{\partial \omega}{\partial x} + v \frac{\partial \omega}{\partial y} - (\omega + f) \frac{\partial w}{\partial z} = 0$$

with perturbations and linearized this becomes

$$\frac{\partial \omega'}{\partial t} + U \frac{\partial \omega'}{\partial x} - f \frac{\partial w'}{\partial z} = 0$$

for the density equation and hydrostatic balance for the perturbation

$$\frac{\partial \rho'}{\partial t} + U \frac{\partial \rho'}{\partial x} + v' \frac{\partial \bar{\rho}}{\partial y} - \frac{\rho_0 N^2 w'}{g} = 0 \qquad \frac{\partial \rho'}{\partial z} + \rho' g = 0$$
derive an expression for w' \Rightarrow





Baroclinic instability Quasi geostrophic equations
Stratified fluid and
$$\beta \neq 0$$
 (Charney 1947)
 $\frac{\partial}{\partial t}Q + \bar{u}.\nabla Q = 0$ $Q = \nabla^2 \psi + \beta y + \frac{\partial}{\partial z}(S\frac{\partial \psi}{\partial z})$ $S = \frac{f_0^2}{N^2}$
 $\frac{\partial b}{\partial t} + \bar{u}.\nabla b = 0$ (at $z = 0, H$; for $w = 0$ and $b = f_0\frac{\psi}{\partial z}$)
perturbations of the form $\psi = \operatorname{Re} A(y,z) e^{ik(x-c)}$
 $(U - c)(\frac{\partial^2 \tilde{\psi}}{\partial t^2} + \frac{\partial}{\partial z}(S\frac{\partial \tilde{\psi}}{\partial z}) - k^2 \tilde{\psi}) + Q_y \tilde{\psi} = 0$ $0 < z < H$
 $(U - c)\frac{\partial \tilde{\psi}_z}{\partial z} - \frac{\partial \tilde{\psi}}{\partial z} = 0$ $z = 0, H$
As before, integrate by parts and multiply by the complex conjugate to obtain the condition
 $-c_i \int_{y_1}^{y_2} \left\{ \int_0^H \frac{Q_y}{|U - c|^2} |\phi|^2 dz + \left[\frac{SU_z |\tilde{\psi}|^2}{|U - c|} \right]_0^H \right\} dy = 0$
critical layer when $U - c = 0$ ==>

$$-c_i \int_{y_1}^{y_2} \left\{ \int_0^H \frac{Q_y}{|U-c|^2} |\phi|^2 dz + \left[\frac{SU_z |\tilde{\psi}|^2}{|U-c|} \right]_0^H \right\} dy = 0$$

Instability if

 Q_y changes sign, Q_y is the opposite or the same sign of U_z at resp. z=0,H $Q_y = 0$ and U_z has the same sign at the two boundaries





Arnold-Blumen theorem Consider the potential vorticity equation $\frac{\partial}{\partial t}Q + \bar{u}.\nabla Q = 0 \qquad Q = \nabla^2 \psi + \beta y + \frac{\partial}{\partial z} (S \frac{\partial \psi}{\partial z}) \qquad S = \frac{f_0^2}{N^2}$ with J(a,b) the Jacobian $\frac{\partial}{\partial t}Q + J(\psi, Q) = 0$ $J(a, b) = \frac{\partial a}{\partial x} \frac{\partial b}{\partial y} - \frac{\partial b}{\partial x} \frac{\partial a}{\partial y}$ For stationary flows J(a,b)=0, i.e there is function f with $Q=f(\psi)$. These can be coherent structures, stationary flow platterns etc. If the structure has a uniform translation velocity c, then we have with respect to the moving frame of reference $\psi = \psi(x - ct, y)$ and functional $f \qquad Q = f(\psi + cy) \qquad f$ stable or unstable?

$$\frac{\partial}{\partial t}L(\phi) = 0 \qquad L(\phi) = \frac{1}{2}\int_{\Omega} \left[(\nabla\phi)^2 + S\phi^2 + \frac{1}{f'}(\nabla^2\phi - S\phi)^2 \right] d\Omega$$

if $L(\phi)$ definite positive/negative

 \Rightarrow L~ $||\phi||^2 =$ conserved in time

sign of f determines stability, i.e. increase or decrease in energy of the system

 $Q = \mathbf{f}(\psi + cy) \quad \mathbf{f} \text{ stable or unstable?}$ Perturbation of ψ $\psi(x, y, t) = \overline{\psi}(x - ct, y) + \phi(x - ct, y, t)$ relation for the perturbation ϕ $\frac{\partial}{\partial t}(\nabla^2 \phi - S\phi) + J(\overline{\psi} + cy, \nabla^2 \phi - S\phi - f'\phi) + J(\phi, \nabla^2 \phi) = 0$ Consider the formal stability of \mathbf{f} (note $\mathbf{f'} = \partial \mathbf{f}/\partial \psi = \partial Q/\partial \psi$) multiply
with $-\phi$ integrate over the domain, suppose the domain is closed $\frac{\partial}{\partial t} \int_{\Omega} \frac{1}{2} \left[(\nabla \phi)^2 + S\phi^2 \right] d\Omega + \int_{\Omega} \nabla^2 \phi J(\overline{\psi} + cy, \phi) d\Omega = 0$ = total (kinetic + potential energy) + ~ total enstrophy
using continuity and boundary conditions, multiplication with $(\nabla^2 \phi - S\phi^2)/f'$ and integrating...(see e.g Pedlosky, Springer 1987) $\frac{\partial}{\partial t} L(\phi) = 0 \quad L(\phi) = \frac{1}{2} \int_{\Omega} \left[(\nabla \phi)^2 + S\phi^2 + \frac{1}{f'} (\nabla^2 \phi - S\phi)^2 \right] d\Omega$

$Q = f(\psi + cy)$ f stable or unstable?

The same result can be obtained after transformation to the co-moving frame of reference $\phi(x - ct, y, t) = \hat{\phi}(t)\chi(x - ct, y)$ For stability:

 $f' = \frac{\partial f(\psi + cy)}{\partial \psi} > 0$

This is a *sufficient condition* and its violation is a necessary condition for instability.

In practice this means after a transformation to the comoving frame of reference (x-ct) for stability

Formal stability stronger than normal mode



Pedlosky (book) 1987 Ripa JFM 1991, 1993

Weakness of linear theory

- Only small perturbations
- amplitude grows in time so that nonlinear effect become gradually more important
- Final state is unknown

Advantage:

- simple technique
- mode decomposition is physically comprehensible
- gives a first understanding about hydrodynamics instability

Non-linear methods and weakly nonlinear methods: see

- Godreche and Manneville (Saclay 1990)
- Drazin and Reid Ch 7
- Manneville 1990
- Guyon et al 2001

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